2 Tracking

The tracking system of H1 provides simultaneous track triggering, reconstruction and particle identification for the event topology particular to HERA electron proton collisions. It has been designed to reconstruct jets with high particle densities and to measure the momentum and angles of charged particles to a precision of $\sigma_p/p^2 \approx 3 \times 10^{-3}$ GeV^{-1} and $\sigma_\theta \approx 1$ mrad.

Because of the asymmetry between the electron and proton beam energies many charged particles are produced at small angles θ to the incident proton (forward) direction. To maintain good efficiency for triggering and reconstruction over the whole solid angle, we divide the tracking system between the central and forward regions (see Figure 2). Two mechanically distinct tracking detectors have been constructed, the central (CTD) and forward (FTD) tracking devices respectively. Each is optimised for tracking and triggering in its angular region.

Track reconstruction in the central region (see Figure 3) is based on two large concentric drift chambers, CJC1 and CJC2. The chambers have wires strung parallel to the beam axes (z-direction) with the drift cells inclined with respect to the radial direction. We have measured a space point resolution of 170 μm in the drift coordinate ($r\phi$ plane) and can, by comparing signals read out at both wire ends, achieve a resolution of one percent of the wire length in z. From the signals recorded in these chambers the transverse track momentum is determined and in addition the specific energy loss dE/dx is used to improve particle identification.

Two thin drift chambers, the central inner (CIZ) and central outer (COZ) z-chambers measure the z coordinates with better accuracy than charge division and complement the measurement of charged track momenta in the central chambers. The CIZ chamber fits inside CJC1, and the COZ chamber fits in between CJC1 and CJC2. These two chambers deliver track elements with typically 300 μm resolution in z and 1 to 2% of 2π in ϕ. This requires a drift direction parallel to, and sense wires perpendicular to the beam axis.

Triggering over the full solid angle is based on multiwire proportional chambers with pad readout in the central and forward region and wire readout in the backward direction. They provide a fast first level (L1) trigger decision which can be used to distinguish between successive beam crossings. Furthermore, in the central and forward region, combinations of pads hit in the central inner proportional chamber (CIP), the central outer proportional chamber (COP) and the forward proportional chambers (FWPC) are used to trigger on tracks coming from a nominal interaction vertex. First level track triggers are also derived from the central drift chambers.

Each of the central chambers has an independent gas volume and separate electrostatic shielding. They were built and tested separately, and then assembled and locked to one mechanical unit. The detector walls are thin to reduce photon conversion, and in particular its effect on identification of primary electrons. Neighbouring volumes share a thin (1.5 mm) cylinder of carbon fiber reinforced epoxy with a 50 μm aluminium coating on each side. The complete system of central tracking detectors is housed in a single aluminium cylinder of 4 mm wall thickness. The assembly also provides a precise alignment of the chambers relative to the outside support.

Charged tracks produced at polar angles θ close to the beam axis (forward $\theta < 30°$, backward $\theta > 150°$) no longer traverse the full bending ($r\phi$) plane radius of the solenoid magnetic field. Consequently in the CTD both track pattern recognition and accuracy of track reconstruction deteriorate as the measured track length and the number of precision space points decrease. A way of rectifying this loss is to compensate for the reductions in track length and the number of points in the central region by means of a higher radial density of accurate space points obtained using wires strung in the bending plane closely spaced in z. This is provided by the forward tracking detector which consists of an integrated assembly of three nearly identical supermodules. Each supermodule includes, in increasing z: three different orientations of planar wire drift chambers designed to provide accurate θ measurements, a multiwire proportional chamber (FWPC) for fast triggering, a passive transition radiator and a radial wire drift chamber which provides accurate $r\phi$ (drift coordinate) information, moderate radius measurement by charge division and limited particle identification by measuring the transition radiation produced immediately upstream.

The FTD and CTD are linked together, aligned and surveyed prior to installation into the calorimeter cryostat.

The description of the individual components of the tracking detector below is followed by sections which describe the features common to all drift chambers, namely the readout and pulse shape analysis and the gas systems used for all chambers.

2.1 Central jet chambers: CJC1 and CJC2

2.1.1 Design criteria

The design of CJC1 and CJC2 [3, 4] follows that of the jet chamber used in the JADE experiment at PETRA [5]. The wire pattern characteristic for a jet chamber is a plane of anode sense wires parallel to the beam line with two adjacent cathode planes shaping the drift field. In the CJC's the latter planes are also made of wires.

A jet chamber cell extends azimuthally from the sense wire plane to both adjacent cathode wire planes, and radially over the full radial span of CJC1 or CJC2 each with no further subdivision, as shown in Fig. 3. This minimises the disturbing influence of field shaping wires at the inner and outer radii.

The jet cells are tilted by about 30° such that in the presence of the magnetic field the ionization electrons drift approximately perpendicular to stiff, high momentum tracks originating from the center. This not only gives optimum track resolution, but also leads to additional advantages. The usual drift chamber ambiguity is easily resolved by connecting track segments of different cells. The wrong mirror track segments do not match, as demonstrated in Figure 4. They also do not point to the event vertex and therefore obstruct only small parts of a real track in the opposite half cell. Each stiff track crosses the sense wire plane at least once in CJC1 and in CJC2. From the fine match at the crossing, the passing time of a particle can be determined to an accuracy σ of ~ 0.5 ns. This allows an easy separation of tracks coming from a different bunch crossing. The drifting electrons from stiff tracks arrive at neighbouring sense wires with a time shift of about 100 ns, and therefore produce only negligible disturbance by cross-talk. Every track traverses several regions of uniform driftfield inside the cells. Systematic errors of drift time measurement, which are known to arise in the nonuniform fields near the cathode and sense wire planes, reverse sign at the crossing, and therefore cancel in good approximation.

Adjacent sense wires are separated by two potential wires (see Figures 3 and 4). This reduces both the surface field and the cross-talk by nearly a factor of two as compared to a single potential wire. Most important, it allows to adjust drift field and gas amplification nearly independently. The actual positions of the sense wires are staggered off the nominal sense wire plane by ± 150 μm, such that adjacent wires are pulled by the electric field to definite positions on opposite sides of the plane.

A cell is azimuthally limited by two cathode wire planes, and at the inner and outer radius by the field wires. The cathode wires are set to a voltage proportional to the distance from the sense wire plane in order to create an uniform drift field and hence a constant drift velocity over almost all the cell. The voltages for the cathode wires are supplied by a resistor network (cathode chain) on the adapter cards connected to the cathode wires. The field wires shape the field at the inner and outer end of the cell such that the deviations from a uniform drift field are minimal. The sense wires are connected to a positive voltage and are AC coupled to the amplifiers. The potential wires are set to ground. To prevent ageing of the chambers due to high electric surface fields, the diameters of the potential, cathode and field wires were chosen conservatively large : 127, 180 and 500 μm. This limits the surface field to $\leq$ 2KV/mm. The anodes are 20 μm (25 μm at the cell ends) gold plated tungsten wires with 3 % rhenium, having a resistivity of 300 Ω/m.

The electrostatics of the cells have been studied in detail by computer simulations. Figure 4 shows drift lines and isochrones in CJC1 for a Lorentz angle of 30°. In most of the drift region the electric field is constant to better than 1 %. At the first and the last sense wires the wire geometry produces local distortions of the field which, however, do not exceed 2 %. This introduces only negligible variations of the drift velocity, in particular around the maximum of the drift velocity.

The parameters of the jet chamber are listed in Table 2. All sense wires are read out at both ends and yield via charge division a $z-$measurement.

2.1.2 Mechanics

The volume of each jet chamber is defined by two endwalls perpendicular to the beam line and an inner and outer cylinder concentric to the beamline. The volume has to be gas tight and to support small overpressure with respect to the atmosphere.

The bulk material of the endwalls was chosen to be 10 mm glass fiber reinforced epoxy [6], combining excellent insulation with good mechanical properties. The fact that there are two jet chambers allowed relatively thin endwalls, because the support lengths between inner and outer cylinders are small and thus the bending under the summed wire tension could be kept below 1 mm.

To facilitate installation, insulation and HV testing of all connections, the signal- and HV leads are integrated into the endwall structure by means of multilayer printed circuit (PC) boards. One board (2 mm thick) covers one drift cell. Of its four layers, one provides a nearly complete electric shield of the chamber, while the others make the contacts between the wire feedthroughs and the (signal and HV) connector sockets. A second PC board inside the chamber, 0.8 mm thick, carries strips for shaping the end fields.

Optimum precision of the wire positions is achieved by first gluing 3 mm thick massive brass pins into pre-bored holes in the endwalls, and then drilling precision holes into the brass. The precision of the sense wire positions, ± 15 μm within one cell is determined by small excentric holes in the brass. Details of the wire supports can be found in ref. [3].

The endwalls are kept apart by four cylinders. For the inner and the outer cylinder of CJC1 and the inner cylinder of CJC2 carbon fiber reinforced epoxy (1.5 mm thick) has been chosen because of its excellent mechanical stability (Young's modulus ϵ = 80 kN/mm^2) and very long radiation length (X_0 = 230 mm). The chamber volume forms a Faraday cage in order to be screened against external electromagnetic noise. Since the conductivity of the carbon fibers is not sufficient in all directions, an aluminium coating of the inner and outer surface was mandatory. The thickness of 50 μm of the Al surface liner was a compromise between electromagnetic screening down to low frequencies (skin depth at 20 MHz in Al is $\approx$ 20 μm) and minimum material. The outer cylinder of CJC2 is made of aluminium (4 mm thick) and is the main support vessel for all tracking detectors. It has feet which slide on rails positioned on the inner warm wall of the liquid argon cryostat and which are the mechanical link to the rest of the H1 detector. At both ends the Al cylinder has thicker flanges (Δr = 12 mm), which are machined to 0.1 mm tolerances in order to house the endwalls precisely. At final assembly the stability and shape of the Al cylinder is guaranteed by the insertion of the endwalls.

	unit	CJC1	CJC2	CIZ	COZ
active length Δz	mm	2200		1800	2160
active zone starts at z	mm	-1125		-1080	-1105
total length Δz[1]	mm	2500		2467	2590
mechanical length Δz	mm	2230		2254	2230
inner radius R_i	mm	203	530	173.5	460
outer radius R_o	mm	451	844	200	485
active radial length	mm	224	296	20	24
number of cells (rings)		30	60	15	24
number of sense wires per cell (ring)		24	32	4	4
number of potential wires per cell (ring)		50	66	3	6
number of field wires per cell		10	10		
number of cathode wires per cell		49	65		
sense wire distance	mm	10.16		5.6(7.0)	6.0
maximum drift distance at R_i	mm	22.9	28.5	61.25	45
maximum drift distance at R_o	mm	44.5	43.1		
sense wire tension	N	0.65		0.2	0.9
mean wire length	mm	2200		1120	2970
drift velocity [2]	mm/μs	≈ 50		52	48.5
$\sigma_{r\phi}$	mm	0.170		28	58
σ_z	mm	22		0.26	0.20
double hit resolution	mm	2		4.6	3.5

Table 2: Central jet and $z-$ chamber parameters.
[1 Incl. preamplifiers; [2] for the gas mixtures given in Table 7.

2.1.3 Calibration and performance

The accurate measurement of the track parameters is limited by the intrinsic resolutions, namely $\sigma_{r\phi} \approx 150$ μm for drift time measurements with a gas mixture of Ar-CO_2-CH_4 (89.5 : 9.5 : 1.0), $\sigma_z \approx 1\%$ of the wirelength for the charge division measurements (limited by pulseheight and noise), and $\sigma_{dE/dx} \approx 6\%$. With this gas the drift velocity at nominal HV is 50 mm/μs.

A large variety of constants is involved to determine the coordinates of a hit from the timing (t) and pulse-integral (Q) of a drift chamber signal (see Section 2.4.5 for (Q,t) analysis). We distinguish overall and wire dependent constants.

The overall constants – event timing, average drift velocity and average Lorentz angle – are sufficient to determine the track parameters with moderate accuracy, e.g. $\sigma_{r\phi} \approx 350$ μm. They are determined and continuously monitored by fitting them as additional parameters to long, high momentum tracks (see Section 2.1.4). The use of an average effective wire length and gain gives resolutions of $\sigma_z \approx 5$ cm and $\sigma_{dE/dx} \approx 17\%$.

The wire dependent constants – timing, signal propagation, absolute gain, relative gain and position of both wire ends – have been determined in two steps. The first step consists of the evaluation of data where the 4 odd/even wires of an 8-channel amplifier card on both chamber ends are pulsed separately and simultaneously. This gives the relative timing of the 4-wire groups, the timing difference, and the relative gain at the two wire ends. The start values for the effective wire length are determined, apart from an overall factor. In the second step the residuals of hits for reconstructed and fitted tracks are evaluated to obtain the absolute values of the individual wire constants. This improves the resolution to $\sigma_{r\phi} = 170$ μm, $\sigma_z = 2.2(3.3)$ cm for protons (pions) and $\sigma_{dE/dx} = 10\%$ (see Figures 5 and 6 and Table 2).

The resolution achieved in the $z-$coordinate depends on the deposited ionization (Figure 5). Data from ep collisions were analysed [7]. The dependence of the specific ionization on the particle momentum is show in Figure 6. There are clearly visible bands for pions, proton and deuterons , where the latter two particle species are mainly produced by protons colliding with the residual gas in the beam pipe.

2.1.4 Track reconstruction

2.1.4.1 Track parametrization Tracks of charged particles are characterized by the five helix parameters: the signed curvature ($\kappa = \pm r^{-1}$, positive if the direction ϕ coincides with a counter-clockwise propagation along the circle), the signed closest distance from the $z-$axis in the $(x, y)-$plane d_{ca}, positive if the vector to the point of closest approach and the trajectory direction form a right-handed system), azimuth and polar angle (ϕ and θ), and the $z-$position (z_0) at the point of closest approach. The first three parameters are determined by a circle fit to the data in the xy-projection using the non-iterative algorithm of Karimäki [8]. The circle equation is expressed in polar coordinates (r, φ) as

$$\frac{1}{2}\kappa\left(r^2 + d_{ca}^2\right) + (1 - \kappa d_{ca})\, r \sin(\phi - \varphi) - d_{ca} = 0$$

For a track traversing both rings of the CJC a single parametrization for both rings is usually sufficiently accurate. Due to multiple scattering in the material between the two rings (2 % X_0) for some tracks two separate sets of parameters are determined, which are constrained to join in a point between the two rings under an angle compatible with the mean multiple scattering angle.

The other two parameters are determined by a linear least-squares fit of $z_i = z_0 + S_i^{xy}(dz/dS)$, where S_i^{xy} is the track length for the point z_i in the xy-projection, with $S^{xy} = 0$ at d_{ca}. The slope parameter (dz/dS) determined by the fit is converted to the angle θ by $\theta = \arctan(1/(dz/dS))$.

The track finding is followed by further modules to determine the xy-vertex for a given run, and to perform track fits to the primary and secondary vertices. The track parameters in this stage are κ, ϕ and θ, together with the xyz-coordinates of the vertex and the error matrix.

2.1.4.2 Track finding Two versions are used for the track finding and fitting. A fast version, efficient for tracks originating from the primary vertex with a momentum > 100 MeV/c, is used on the fourth trigger level filter farm (see Section 5.5 of reference [1]) for background rejection and fast classification of events. It is roughly a factor ten faster than the standard version, which is efficient for all kinds of tracks and is used within the normal reconstruction.

The first phase of track finding, the search for short track elements (curvature negligible), is done independently in the angular cells with 24 (CJC1) and 32 (CJC2) radial wires. Within angular sectors track-element finding does not depend on parameters like the Lorentz angle or the drift velocity. However accurate values of these parameters are necessary when hits from more than one angular cell are combined. Track finding is based almost exclusively on drift time data in the xy-plane and includes removal of outliers, which would distort the circle fit. Only in a later stage the measured z-values are used; here it is again necessary to remove outliers before the data are fitted.

For the fast track finding it is sufficient to determine the bunch crossing time t_0 for an event from the threshold in the drift time histogram. The first step involves the search for track elements defined by three hits within angular cells found on three wires with a wire distance of two. The algorithm starts by trying all pairs of hits at wires $n \pm 2$ (n = wire index). Possible values of drift distances $\bar{d}^n$ at the wire n are calculated by $(d_i^{n-2} + d_k^{n+2})/2$ and/or $|d_i^{n-2} - d_k^{n+2}|/2$ (i, k = hit indices) and stored in a list, if the direction of the pair does not deviate too much from the radial direction. Very dense regions with many hits are not analysed. This list is then compared with the measured values d_j^n and for small differences $|d_j^n - \bar{d}^n|$ the indices of the hits at the three wires are stored as a possible track element. From these hit triplets the curvature κ and the angle ϕ_m can already be determined with sufficient accuracy assuming $d_{ca} \equiv 0$. The parameter ϕ_m is the track angle at the mean radius r_m of the CJC1 and the CJC2, respectively. No attempt is made at this stage to resolve the drift sign ambiguity; triplets with a large value of $|\kappa|$ are rejected, otherwise both solutions are kept. A z-value and a value for dE/dx are assigned to the triplets from the median of the three single-hit values and later used to determine the z-slope and -intercept z_0 and the mean dE/dx value of the track.

Tracks from the origin cluster in the plane of the two parameters κ and ϕ_m of the triplets, with a width of typically only one degree for ϕ_m. These clusters are sufficiently separated, that after finding them a first track definition is achieved. The coordinates of triplets within the clusters are then used in a circle fit, now allowing $d_{ca} \neq 0$, and by a z-fit. Track candidates with large $|d_{ca}|$ and $|\kappa|$ values are rejected.

The track candidates are then checked in the order of decreasing number of triplets (decreasing significance) rejecting tracks with several triplets already used before for an accepted track. Drift sign ambiguities are normally resolved at this stage, since most tracks traverse several cells and the correct solution has a much larger number of triplets than the wrong one. The fast track finding is in general efficient enough to allow sensitive recognition of background or classification of physics events.

The standard track finding starts from the results of the fast track finding and first improves the time reference value t_0 for an event by fits to the drift length values of long tracks. For a given track the values of the circle parameters are used to calculate the expected drift length for all possible wires. The difference between the measured and the expected drift length is then calculated for all hits, taking into account the sign of the drift length. To these differences an expression is fitted, which in addition to a parabolic dependence on the track length (to allow for a small inaccuracy in the track parameters) parametrizes the effect of a t_0 difference (which depends on the sign of the drift length) and of a small difference of the drift velocity. This fit yields an accurate value for t_0 and allows in addition to detect changes of the drift velocity. At the same time the method improves the definition of tracks, since often the range of the hits found is extended. Another circle fit is performed to all long tracks traversing more than one cell (drift sign ambiguity resolved). If the χ^2 value of the track fit (after removing single bad hits eventually) is acceptable the complete set of track parameters is stored already at this stage, the hits assigned to the track are flagged and not used in the following steps.

The first phase of standard track finding again searches for track elements defined by three hits, but now on adjacent wires. All possible wires are considered, except for very dense regions. Triples with common hits are connected by pointers and when all hits of an angular cell are analysed, chains of hits are extracted. These chains of hits are then checked by a fit to the drift times for effects like kinks; eventually long chains of hits are split into two shorter chains. For long chains the staggering of wires sometimes allows already to resolve the drift sign ambiguity; otherwise both solutions are kept. Chains accepted at this stage are stored as track elements with parameters from the fit.

Short track elements are merged to larger ones first within the same or neighbouring angular cells, then within one ring and lastly from both CJC1 and CJC2. The merging algorithm starts with a comparison of pairs of track elements with similar helix parameters. If the distance between them is not so large that they could belong to the same track, a χ^2-fit in the xy-plane is performed. The list of all acceptable pairs is sorted in the order of an increasing "distance", assigned to each pair. The distance is constructed from the χ^2-value and other parameters (e.g. the length of the track element). The list of pairs is then checked sequentially, starting with the "close" pairs. Two elements from a pair are combined to a new (longer) track element, if acceptable. If in this sequence one element of a pair has already been used in the construction of a new element, the fit to the modified element(s) is repeated and rejected eventually. By this process longer and more accurate track elements are formed, starting with the simple and clear cases, thus avoiding with high probability a wrong combination of short track elements.

For the final improvement of the track finding efficiency and precision the expected drift length is calculated for all possible wires and for all track elements ordered by their length. Hits at the expected wires which are not already used by another track are collected. The differences between measured and expected drift length are analysed to reject incompatible hits. Tracks found are allowed to contain rather large gaps of several wires, since parts of tracks may be invisible, especially within jets, due to the limited double track resolution. The fits for the track parameters are repeated using all acceptable hits.

Very short track candidates are rejected, unless they start with the first few wires of a ring. The energy loss dE/dx for a given track is determined from the mean of single-hit values $1/\sqrt{k_i} = 1/\sqrt{(dE/dx)_i}$, excluding hits which are close to another track. An analysis based on a likelihood method has improved the dE/dX to below 10 % (see [9]).

2.1.4.3 Vertex determination The $e-p-$interaction vertex region in the xy-plane extends over a few hundred μm with a rather stable mean position for a sequence of runs. The mean vertex coordinates (x_v, y_v) are determined using long high momentum tracks with a small value of d_{ca} from a few hundred events and minimizing the sum of squares of the distance of the tracks to the vertex.

The known (x_v, y_v) position of the run vertex can be used as a constraint to improve the parameters of tracks originating from this vertex, if the effect of multiple scattering in the beam pipe and the CJC wall for low-momentum tracks is taken into account. Since the standard deviation of the curvature value is roughly inversely proportional to the track length squared, the track precision is significantly improved by this vertex fit in the xy-plane. A z-value of the primary interaction vertex in an event is determined from all tracks fitting to the xy-vertex. The polar angle θ for these tracks is changed accordingly .

Within the standard reconstruction program a search is made for neutral particles decaying into a pair of oppositely charged particles with tracks in the CJC; in addition to K^0_S, Λ and $\bar{\Lambda}$ particles also e^+e^--pairs from conversion are found by this module. Candidate pairs are determined using simple geometrical cuts. For each candidate pair a fit is performed applying geometrical (common secondary vertex of the charged particles) and kinematic constraints. Use is made of the known position of the primary vertex. Momentum balance perpendicular to the direction of the neutral particle is used as kinematic constraint, but no masses are assumed. For a very small opening angle of the pair the transverse momenta in the xy-plane are both constrained to zero, to improve the stability of the fit for e^+e^--pairs. Pairs with an acceptable χ^2-probability are stored.

At later stages of the analysis alternative methods for reconstructing secondary vertices are also employed (see references [10, 11] and Figure 33 of reference [1]). Kalman filtering techniques have also been shown to be useful [12].

2.2 Central $z-$ chambers

The central inner and outer $z-$chambers (CIZ, COZ) surround the inner half of the jet chamber and complement the measurement of charged track momenta in the latter chamber. These two chambers deliver track elements with typically 300 μm resolution in z, which can be linked to those obtained from the jet chamber for the final accuracy on both the longitudinal as well as the transverse momentum components. The polar angles covered by CIZ and COZ are $16° < \theta < 169°$ and $25° < \theta < 156°$, respectively. Since the CIZ uses the inner carbon fiber wall of the CJC for closing its gas volume, and the COZ uses the outer carbon fiber cylinder for its basic structural element, the thickness of both chambers could be kept small, namely 0.6 % X_0 for CIZ and 0.7 % X_0 for COZ in the active zones and 1.2 % and 1.5 %, respectively averaging over the cell wall material. Furthermore the total amount of dead zones in azimuth imposed by readout channels and wire supports is only 7.7 % and 5.3 % of 2π respectively. The basic parameters of both chambers are given in Table 2 and the gas mixtures used are given in Table 7. A first level, background rejecting trigger [13] combines CIZ and COZ hits to trigger on straight tracks pointing to the interaction region (see Section 5.3.1.7 of reference [1]).

2.2.1 CIZ

For CIZ a laminar construction technique similar to that described below for CIP was used, starting from a steel mandril with an inner diameter of 347 mm. Successive layers include 25 μm Kapton with a 2.5 μm Al coating for electrical shielding, a 6 mm thick Rohacell [14] cylinder with its outer surface machined and polished to produce 16 flat surfaces forming a regular polygon in cross-section (see Figure 3), and a 25 μm Kapton foil with 10 μm Cu field forming strips on both sides. The 15 independent cells are separated by printed circuit boards, 1.6 mm thick with 5 μm Cu on each side serving as cathode planes. The cells are closed electrically with another Kapton foil identical to that on the bottom of the cell, here backed by 1 mm Rohacell. The end flanges of the CIZ are sealed against the CJC end plates with O-rings. Further constructional details, e.g. on the specially designed wire feedthroughs, can be found in references [15, 16, 17].

Figure 7 shows the geometry of the drift cell. The sense wire planes are tilted by 45° with respect to the normal to the chamber axis, with the first nine cells in the backward direction tilted backward and the last six in the forward direction tilted forward, i.e. following the direction of the tracks crossing the respective cells. As explained in ref. [15] this tilt produces a distortion of the equipotential lines resulting in a non-uniform distribution of the charge collected on the four wires and an equivalent tilt of the isochrones. This unusual wire arrangement solves the left-right ambiguity automatically without a need for wire staggering and furthermore eliminates the dependence of the resolution on the crossing angle. The wires are soldered to both side walls of a 23 mm wide cable channel at $\phi = 0°$. Here the signal wires are connected to line drivers and the potential wires to HV cables. The line drivers provide the impedance matching to the preamplifiers mounted on the end plate. A high resistivity alloy (Elgiloy [18], 3 kΩ/m) was selected as sense wire material (Ø 20 μm) to improve the measurement of the ϕ coordinate along the wire by charge division. The potential wires are made from Au (Ø 120 μm). To save space the HV cables to the electrodes and cathodes are buried in the Rohacell chamber body and the miniaturized 10 MΩ resistors (1.25 mm $\times$ 2 mm $\times$ 0.5 mm), which supply the field forming strips are embedded in the printed circuit board chamber partitions. The structure of the field shaping electrodes is indicated in Figure 7. For the gas mixture listed in Table 7 the chamber is operated with a cathode voltage of 4500 V, a potential wire voltage of 2250 V and a field gradient of 53 V/mm.

Since the CIZ is the drift chamber closest to the interaction point, a dedicated current monitoring system (see ref. [19] for details) was included into each potential wire supply line. It allows to measure the currents in the nA range. These wires control the gas amplification in the chamber. In this way the activity introduced by interaction products or stray beam can be monitored. Typically we found 10 nA current increase per ring for a luminosity of 20 mb^{-1}s^{-1}. This corresponds to an accumulated charge of 10 Cb/m per wire for an integrated luminosity of 100 pb^{-1}.

Apart from a narrow strip near the cell walls the chamber efficiency was measured to 98 % in test beams at PSI [16]. From test beam data the resolution was found to be $\sigma_z = 320\ \mu$m independent of the drift distance and the crossing angle in the range $10° < \theta < 110°$. These results could be confirmed with cosmics ray data, where central jet chamber tracks were extrapolated into the z-chambers and then linked to the corresponding track elements. The average deviation from a straight line fit (in the $r - z$ plane) is $\sigma_z = 260\ \mu$m for CIZ internal track elements and 400 μm for linked tracks. For the $\phi-$projection a resolution of 2.4 % of the wire length was measured. Double pulses can be resolved, if their separation exceeds 90 ns, which converts into 4.6 mm spatial separation in z [16].

2.2.2 COZ

This chamber was also built on a Rohacell body with the cross-section of a regular 24-edge polygon (Figure 3), but resting on a cylinder of carbon fiber reinforced plastics. The Kapton foils with field shaping copper strips were glued to the Rohacell surfaces. Guided by a mechanical positioning device the wire supporting rods (G10 with Cu strips, double sided) were placed and soldered to the Kapton foil. Between these rods planar cathodes were introduced made of G10/Cu with holes to enable the gas flow through the chamber. The top cover of the drift cell structure consists of a Kapton-Rohacell sandwich which is fixed at the cathodes. The chamber has a cylindrical shape due to its G10-Cu gas cover held by the endflanges. Further details can be found in references [17, 20]. Figure 8 shows a schematic view of the COZ. The dead zones for the wire readout are distributed in azimuth which allows a corresponding distribution of the preamplifiers at the end flanges and minimises the dead area of the chamber. The anode signals are transmitted by twin readout lines (signal-ground signal, length 20 to 120 cm) from the wire ends to the preamplifiers on both chamber ends.

Each drift cell is 24 mm high, the maximum drift length is 46 mm which limits the drift time to about 1 μs. Each cell has four sense wires (Stablohm [18], Ø 48 μm, 0.6 kΩ/m) in the symmetry plane of the cell and three pairs of potential wires (CuBe, Ø 127 μm). The wire feedthroughs in the supporting rods are kept in their nominal position to about 30 μm (σ). No wire stagger is implemented. Mirror tracks can be removed in the analysis since they do not point to the vertex.

The COZ is typically operated with a cathode voltage of 3000 V, a potential wire voltage of 2250 V and field gradient of 82 V/mm. For the gas mixture listed in Table 7 this gives a drift velocity of 48.5 mm/μsec, as determined from tracks crossing the sense wire plane and the cathode plane, respectively.

Inefficiencies along the cell walls and other performance parameters were studied in test beams (3 GeV electrons at DESY and low energy pions and electrons at PSI, see references [21, 20]). Apart from a small region near the sense wire feedthroughs the efficiency was determined to be 98 % over the full drift cell. For a 90° crossing angle the resolution measured at HERA is about 200 μm, deteriorating to 500 μm for low crossing angles. The azimuthal angle is determined by charge division to an averaged accuracy of 7.2 °, i.e. 2 % of the wire length. Double pulses can be resolved if their separation is larger than 70 ns which corresponds to 3.5 mm distance. For a discussion of the optimum method to resolve double tracks and a comparison of different algorithms for (Q, t) analysis we refer to [20, 21, 22].

2.3 Forward tracking detector

The forward tracking system is designed to provide an accurate measurement of charged particles in the forward direction (momentum resolution $\sigma_p/p^2 < 0.003$ GeV^{-1} and track angular resolution $\sigma_{\theta,\phi} < 1$ mrad), track information on individual particles within jets, electron identification by means of transition radiation detection and a fast forward ray track trigger. Details about track finding and fitting can be found in [23].

The layout of the FTD is illustrated in Figures 9 and 10. Key parameters are listed in Table 3. The drift chambers have different wire geometries - the planar ones contain parallel wires whereas the radial ones have wires radiating outwards from the beam pipe – all wires being strung perpendicular to the beam direction. The planar module consists of three drift chambers, each four wires deep in z and rotated at 60° to each other in azimuth. It is located closest to the central tracker in each supermodule, since its homogeneous spatial precision in x and y is most suitable for linking to tracks in the center. For practical reasons the FWPC (Section 2.5.1) is mounted directly behind the planar drift chambers in order to share the same gas mixture and maximise the geometrical trigger efficiency of the FTD. After the FWPC the particles traverse a transition radiator consisting of 400 polypropylene foils contained in its own gas volume. The transition radiation photons pass through a thin mylar window and are detected in the radial chamber which produces up to 12 accurate space points from ionization drift timing and charge division. To improve double track resolution the second and third radial modules are rotated by 3.75° and 2.5° (1/2 and 1/3 of a wedge) relative to the first. The interleaving of planar and radial chambers provides the optimum lever arm for momentum measurement.

The individual chambers were assembled and tested separately. The components for a single supermodule were installed into a three section tank consisting of aluminium outer cylinders ($\O_{max}$ = 1700 mm) and glass free carbon fiber inner cylinders ($\O_{min}$ = 243 mm, 4 mm thick, lined with Al foil), each tank section forming an independent gas volume and electrically isolated environment. Each chamber is bolted to the rigid central U-shaped outer cylinder using a set of precision dowels for alignment. Assembly was carried out on high quality surface tables with dimensional tolerances kept to $< 30\,\mu$m throughout the build sequence. After commissioning each supermodule on a cosmic ray test facility the three supermodules were then bolted together, separated by thin gas tight Kapton windows, and the end faces closed with stiff plates made from a sandwich of 1.2 mm thick Al alloy and 17.6 mm thick Nomex honeycomb [24]. The final alignment of the whole FTD was measured using cosmic rays after installation into the H1 experiment. Water at constant temperature (±1 °C) is circulated around each tank section through copper pipes in order to maintain dimensional stability and provide cooling for the preamplifiers. As well as maintaining the relative alignment of the tracker elements and support for the various services – water, gas, cables, preamplifiers, position monitors etc., the tank provides an electromagnetically sealed environment and serves as the common ground for the chambers. The HV and signal cables access the tracker volume via the outer cylinder using hermetically sealed feedthroughs where they are grounded. The HV cables are also filtered before entering the tank.

Three different gas mixtures are used, two working gases for the chambers and one purge gas for the transition radiation (TR) volumes. Gas is fed into each supermodule volume via the U-shaped channels in the outer cylinder, two feed pipes and one pipe for local pressure sensing, a total of nine pipes per supermodule. Gas tightness is maintained by rubber O-ring seals at the outer and inner flanges. The gas is supplied at atmospheric pressure from three computer controlled closed loop gas circuits (see Section 2.6) which maintain gas purity and provide the accurate pressure control, $\pm 10\,\mu$bar required in order to prevent damage to the fragile TR windows. During HERA operation the oxygen level in all volumes has been kept to < 50 ppm.

The whole tracker is mounted on four insulated feet and rests on the cryostat rails in stress-free condition. It is electrically isolated from the central tracker and the cryostat.

Parameter	unit	Radials	Planars
number of cells per supermodule		48	32
inner (outer) active radius	mm	150 (750)	$\approx$ 150 (750)
total number of sense wires (per cell)		1728 (12)	1152 (4)
sense wire diameter (resistance)	μm (Ω)	50 (450)	40
sense wire material		Stablohm[1]	W (Au plated)
sense wire spacing Δz (stagger)	mm	10 (0.28)	6 (0.30)
sense wire tension	N	1.75[2]	1.20[2]
total number of grid wires (per cell)		1584 (11)	2880 (10)
grid wire [Cu-Be(2%)] diameter	μm	125	125
grid wire tension (surface field)	N (kV/cm)	2.80[2] (170)	4.00[2] 135)
sense voltage	V	+2228	+1575
bulk (grid) field gradient	kV/cm	1.2 (-6.9)	1.0 (-5.0)
maximum drift distance ($B = 0$ T)	mm	50	28
drift velocity ($B = 0/1.14$ T)	mm/μs	$\sqrt{3} \times 37/37$	43.5/42
Lorentz angle ($B = 1.14$ T)	$^\circ$	45	41.8
z planar (x), module 0/1/2 [3]	mm	1324.4/1746.4/2168.4	
z planar (u), module 0/1/2 [3]	mm	1367.0/1789.0/2211.0	
z planar (v), module 0/1/2 [3]	mm	1409.6/1831.6/2253.6	
$z-$ radial, module 0/1/2 [3]	mm	1593.0/2015.0/2437.0	
$\sigma_{r\phi}(\sigma_r)/\sigma_{x,y}$ from track segments	μm (cm)	180 – 200 (3)	150 – 170
double track resolution	mm	2	2

Table 3: Forward tracker drift chamber parameters and positions.
[1] alloy from ref. [18]; [2] 60 % of the limit of proportionality; [3] position of first wire in plane.

2.3.1 Planar drift chambers

Each chamber is constructed as a self-supporting module containing 32 drift cells of identical rectangular cross-section with wire lengths between 460 mm and 1410 mm as shown in Figure 10. The chamber walls are formed from two circular discs with an outer diameter of 1.57 m and a central aperture of 280 mm diameter. They are composed of a low mass composite of Fibredux skinned Nomex honeycomb 3.4 mm thick, manufactured to be parallel and flat to within 100 μm. A 0.8 mm thick double sided printed circuit board carrying the drift field forming strips and voltage bus on opposite faces is bonded onto one side of the honeycomb laminate. the drift cells are defined by parallel sets of copper clad PCB's, 0.8 mm thick by 32 mm high, mounted perpendicularly and bonded at 57 mm intervals into precisely machined slots in the honeycomb panels, resulting in a multiple box section structure of high mechanical strength and rigidity. The vertical PCB's constitute the cathode planes and define the maximum drift distance as 28.1 mm (for $B = 0$). Each cell contains four sense wires uniformly spaced in z and staggered alternately 300 μm each side of the median plane of the cell. Each sense wire is surrounded by four grid wires Cu-Be arranged on a 6 mm square matrix. Significant benefits arise from the double grid design including reduced cross talk, lower wire tensions, improved cell isochronicity, and reduced grid wire surface fields. All wires are crimped under tension in pins which are held in position by means of high precision extruded Noryl templates at each end of the cell. The principal source of error in the wire position (≈ 20 μm) arises from the inherent inaccuracies in the crimping technique. The cell ends are closed by PCB's containing electrodes which cleanly terminate the electrostatic field of the cell. Aluminium foils covering the outer surfaces and connected to the tank provide electromagnetic isolation between the individual planes. A set of precision dowels fix the relative orientation of each plane (to < 0.06 mrad), the orientation of the planar supermodule with respect to the FWPC and the planar chamber/FWPC combination with respect to the tank.

The cell electric field distribution is controlled by seven different voltages: the sense voltage defines the gas amplification, the central strip voltage affects the sense field homogeneity, four drift strips and the cathode voltages determine the field gradient. The grid wires are grounded. All voltages are supplied directly from the HV supplies, after suitable fan out, without the use of resistor chains at the chamber. Field optimization and chamber operation are considerably aided by the fact that the double grid geometry produces a strong decoupling between the sense field (gas amplification) and the drift field. The operating conditions of the chambers for the gas mixture given in Table 7 are listed in Table 3.

The outer end of each sense wire is AC coupled into a current sensitive preamplifier (two drift cells per preamplifier) and the signals transmitted via 40 m of 50 Ω coaxial cable to the FADCs. Pulse profile (Q,t) analysis in the front end data acquisition system yields one drift time coordinate measurement perpendicular to the sense wire and one pulse integral measurement. Resolutions achieved on $e-p$ data are typically $150-170\,\mu$m for the single point spatial resolution and < 2 mm for the double track resolution.

2.3.2 Radial chambers

The radial wire drift chambers cover 360° in ϕ with 48 separate sectors of 7.5° width. Each sector is a drift cell having 12 sense wires staggered alternately 287 μm each side of a plane which bisects the sector. The sense wires, which are all parallel within one of these cells, are separated by 10 mm. Between adjacent sense wires, and positioned on the plane which bisects the sector, are field wires parallel to the sense wires and half way between them. All these wires are supported by crimp pins. At the small radius end (r = 152 mm), the crimp pins are mounted in a cylindrical Noryl hub, and at the large radius end (r = 760 mm), in Noryl templates precision bonded into the cylindrical wall of the composite structure which contains the whole 48 cells of the radial chamber as one rigid unit. The structure of these radial drift chambers has been described in references [25, 26, 27].

The wedge-shaped drift cells are separated from each other by cathode planes which consist of voltage graded copper strips on each side of thin paper-epoxy material (PCB technology). The electrostatic field cage for each drift cell is completed by voltage graded shaped conducting strips bonded onto the plane inner surface of the composite structure (for the high z end of the wedge), and onto a complex window assembly, described below, which is affixed as a lid to the composite structure (for the low z end of the wedge).

Detailed design of this window, forming the plane surface of the radial chamber towards low z was determined by the requirement to detect the transition radiation (TR) entering the radial drift chamber. The X-ray component of TR produced by an ultra relativistic charged particle contributes to an enhanced track ionization, hence to enhanced charge collected on one or more of the sense wires, provided that all ionization deposited anywhere in the cell is collected onto the sense wires and not onto field wires. The window of the radial chamber is thus designed to be as X-ray transparent as possible, and to ensure maximum X-ray detection efficiency as close as possible to it inside the drift cell. Because of the imperfect nature of the field grading close to the V shaped strips, ionization deposited within about 2 mm of the window cannot be collected onto the first sense wire. Such a loss of X-ray sensitivity is significant at the TR entry (low z) side of the radial chamber, where most of the X-ray photons photo-ionize the chamber gas. For this reason the V shaped strips to create the drift field are of aluminium on mylar and are supported on Rohacell [14] spacers which position them 5 mm from the thin mylar window which isolates the chamber gas volume. The effect of this window assembly on the electrostatics is to move the drift field inhomogeneities out of the sensitive gas volume. Then at the mylar wall closing the gas volume the drift field is uniform and parallel to the surface, except directly opposite the sense wire. Charging effects on the mylar window are then minimal, and the ionization collection efficiency on the first sense wire is optimal right to the edge of the gas volume.

Because all the sense wires are in the radial direction, a coarse determination of the radial position of a track may be made from charge division if a wire is read out at both ends. However it is not physically possible to have preamplifier cards at the small radius end. For this reason the sense wires of one 7.5° sector drift cell are connected at the inner hub to the sense wires of another 7.5° sector drift cell, actually 105° away in azimuth, so that when sense wires are read out at the outer radius charge division is possible along this double length of radial wire. Current sensitive preamplifiers are at each end of these sense wire pairs, each channel of which drives approximately 40 m of cable to the FADC system. Pulse profile (Q, t) analysis gives the drift coordinate perpendicular to the sense wire plane, and two pulse integral measurements Q_L and Q_R from the two ends give the radial position by charge division.

The spacing in the z direction between the sense wires of the radial chambers, between the three modules, and the sets of planar drift chambers and the radial drift chambers may be seen from Table 3. Concerning the azimuthal position of the radial chambers, the plane which bisects a 7.5° sector cell (and about which the sense wires are staggered) is at $\phi = 3.75°$ in the first module, at $\phi = 7.5°$ in the second module and at $\phi = 6.25°$ in the third module. The resolution achieved with the 50 % argon, 50 % ethane gas mixture used so far is $150 - 200\ \mu$m. The gas mixture which is intended to use for optimal detection of transition radiation is given in the following section.

2.3.3 Transition radiators

A passive array of polypropylene layers provides a sufficient number of dielectric interfaces for useful transition radiation (TR) X-ray emission. The dielectric constant, the layer thickness and the mark to space ratio of the polypropylene sheets determine the X-ray yield and the energy spectrum. For the values chosen the spectrum peaks around 6 keV for 20 GeV electrons. The interface between the TR and the radial wire drift chambers has been optimised for transmission of these X-rays. As described in the previous section the radial wire drift chambers are designed and operated both for optimal track point measurement and efficient X-ray detection. The combination of TR and radial wire drift chamber is designed for electron-pion discrimination, at the level of 90% electron acceptance with less than 10% pion contamination, up to 80 GeV for tracks passing through all three modules of the FTD. To achieve this, it is planned to operate the radial wire chambers with a gas containing xenon which has a high photoionization cross-section at 6 keV. A 20 % xenon, 40 % helium, 40 % ethane mixture satisfies the requirements of TR detection with acceptable charged track dE/dx ionization density, and also suitable drift velocity for the requirements of the drift chamber. Data taken with a radial drift chamber in a test beam at CERN have shown that the design discrimination between electrons and pions can be achieved with this gas [28, 29].

The assembly of polypropylene sheets is self supporting but is enclosed in its own gas envelope in order to isolate it from the gases used in the rest of the FTD. The helium-ethane mixture surrounding the polypropylene sheets is chosen to give the same partial pressure of helium as in the radial drift chamber. This is important because the interface is the thin mylar TR window of the radial drift chamber section which could be damaged by pressure differences in excess of about 100 μbar.

2.4 Drift chamber electronics, readout, and front end data processing

2.4.1 Introduction

All drift chambers in H1 are connected to one of the three independent branches of the central data acquisition system (CDAQ). The analog signals are digitized and processed in a number of

Chamber	Branch #	# of crates	# of channels	Raw data [Kbyte]	(Q,t) data [Kbyte]
Radial	5	9	1728	20.5	2.4
Planar	5	6	1152	28.5	4.1
CJC1 and CJC2	4	23	2640	33.2	5.4
COZ	4	1	96	3.41	0.5
CIZ	4	1	60	5.14	0.9
Forward muons θ	6	4	1024		

Table 4: Summary of drift chamber readout data.

front end crates, the trigger connection is based on the H1 standard subsystem trigger controller crate and interface cards and local logic produces and distributes control signals to the front end crates. A master crate collects the complete data from the branch and sends it to the CDAQ. Crates for local data monitoring can be added. Figure 11 shows the general layout of each drift chamber branch.

The drift chambers are distributed between the branches according to position in the detector. The inner and outer jet chambers and the inner and outer z chambers form branch 4 (CTD). The forward radial and planar chambers form branch 5 (FTD). The $\theta-$ and $\phi-$ chambers of the forward muon spectrometer form branch 6 (FMu). Table 4 shows the sizes of the various components, and the typical size of the zero suppressed digitizations (raw data) and processed summary data ((Q,t) data).

2.4.2 Operation of the readout

The analog signals from the preamplifiers mounted on the detector are received by 104 MHz FADC cards which continually digitize and store the data - at this point we are recording data at a rate of over 600 Gbyte/s over all drift chambers. On receipt of a first level trigger (L1) signal the digitization is stopped so that the data recorded in the FADC card memory includes, for each detector, all digitizations which could have occured between the time of the event and the maximum possible drift time for that chamber.

At a second level trigger (L2) signal the full 2.5 Mbytes of raw data for an event is copied by the scanner controller cards into the second level buffer at a speed of 3.3 Gbyte/s. At a third level trigger (L3) signal, the processor card in the FADC crate reads the data from the scanner, and writes an off-line format data bank into an intermediate buffer which contains blocks of significant, zero suppressed data with an event size of approximately 100 Kbyte. The output is written into a triple ported buffer memory on the intercrate connection (VIC8251 [30]). When a complete event is available from all front end crates the master processor collects the data from this buffer memory and writes the complete event to the multi-event buffer of the optical fiber VMEtaxi link (see Section 7.1.2 of reference [1]).

2.4.3 Amplifier and FADC

The sense wires of the tracking drift chambers are connected to amplifiers either at one or at both wire ends. The eight-channel amplifier cards are mounted directly on the chamber vessel. The sense wire and the grounded potential wires serve as differential input. The sense wire is at positive HV and therefore it is coupled to the amplifier via a capacitor (1.5 nF). The sense wires (in some chambers) and amplifier are protected by a spark gap, and a pair of crossed diodes to ground. Each amplifier channel consists of two stages of video amplifiers. The amplification is large enough so that no further amplification is needed on the readout card. This gives optimum noise rejection and minimises the influence of pick-up on the cable to the readout card. The amplifier card has two test inputs which allow the application of test pulse signals to the inputs of odd or even amplifier channels.

The 9520 signals from the drift chamber are digitized by F1001-FADCs [31]. The sampling frequency is 104 MHz, generated by an oscillator phase locked to the bunch crossing clock of the HERA storage ring of 10.4 MHz. The differential outputs of the amplifiers are connected to the FADC cards with multi-coaxial cable of about 28 m length. This cable also carries the power and test lines to the preamplifiers. The FADC-chips used have a resolution of eight bits [31]. The combined signal is fed to the FADC chip through a transformer eliminating DC offsets and via a resistor network that includes feedback of the input signal to the voltage reference, providing a non linear response with 8 bit accuracy for small signal amplitudes and a 10 bit dynamic range. Each FADC-chip is connected to one 256 byte deep memory which serves as circular buffer. During the active sampling phase of the FADC system signals are continuously digitized and stored in the memories. This recording process is stopped by a trigger signal that freezes the history over 2.5 μs in the memory. Sixteen FADC-channels are housed on one F1001-card and up to 16 F1001 cards are housed in a F1000 crate. It has a VME backplane used for fast 32-bit wide readout of the digitized signals from the FADC-memories. The signal risetime at the sense wire is a few ns. It is deliberately degraded by the amplifier band width, cables, and coupling transformer to 18 ns (20 % to 80 % of pulse amplitude) at the input of the digitizing FADC. This is the optimum for a time measurement with a FADC sampling at 100 MHz.

2.4.4 The scanner and the front end processor

In each F1000 front end crate there is an M1070 scanner card that acts as a sample controller for the FADCs, and provides fast readout and zero suppression of the FADC data. The scanner supplies the 104 MHz clock to the FADC cards, and at a L1 trigger gates this clock such that the circular buffers of the F1001 cards contain the required time segment. At a L2 trigger signal it copies the data from the FADCs into a local buffer in a series of synchronous bursts over the VME bus, in this way a transfer speed of 80 Mbyte/s is achieved, and the data for a full crate can be copied within the 800 μs requirement of H1. During the copy the data is compared with programmable thresholds and any significant transition (presently two subsequent time bins above or below threshold) is recorded in the hit table.

At a L3 trigger signal the scanner interrupts the front end processor (24 MHz FIC 8231 [32]) present in each F1000 crate. The interrupt handler reads the hit table from the scanner, calculates the required blocks of raw data, and copies these blocks into a multievent raw data buffer in an off-line format data bank. Each block includes four pre-samples before the hit starts to allow dynamic calculation of the pedestal, and blocks are merged in cases where a block would influence a subsequent block on the same wire. An output bank is written into a multievent output buffer in the memory of the VIC 8251 interconnect card, using the VSB bus connecting the processor and the interconnect, since the VME bus may be occupied by the scanner reading a subsequent event. The input raw buffer and output buffer both typically hold 30–40 events, and this allows derandomization over many events of the large range in processing times caused by localised high track density.

2.4.5 Determination of charge and time (Q, t)

The relevant parameters of a signal pulse from a drift chamber wire are signal timing (t) and the pulse integral (Q). These signal parameters are determined by a program which runs on the

L4 farm (see Section 5.5 of reference [1]). In this way the amount of raw data is reduced by a factor of about five. The zero suppressed data provided by the scanner are treated in several steps. For the CJC, CIZ, COZ and the radial chambers the first three steps consider the data of both wire ends separately, while the further steps use the combined information.

In the $(Q,t)-$algorithm the FADC data are first linearised. The leading edge of a new pulse is found by a search for a maximum in the difference of successive samples above the threshold. The average of the six digitizations before the pulse start is used to evaluate the pedestal to be subtracted from the pulse. Hits from the two ends of a wire are combined if the leading edges differ by less than or equal to two clock bins.

The essential information for the drift time determination comes from those electrons which arrive first at the sense wire and which are produced along the track in the region tangential to the isochrones. These electrons contribute to the sharp rise of the pulse, which is, however, smeared out by diffusion, chamber capacity, and amplifying electronics. The remaining off-tangential electrons arrive at later times and fluctuations of their ionization density influence only the trailing edge of the pulse, otherwise determined by the differentiating electronics.

The drift time is determined by chamber specific algorithms. For the CJC e.g., the time at half the full amplitude is determined by linear interpolation, averaged over both wire ends and used with the average risetime to extrapolate to the arrival time of the first electrons, taken at 10 % of the pulse amplitude. The average pulse consists of about 20 digitizations, while 10.4 MHz noise pulses extend typically over 5 bins and can therefore partly be rejected at the scanner level. The pulse integral is determined by summing some fraction of these digitizations. Most important for the CJC (and radial drift chambers) is the relative error of the integral for the $z(r)$ determination. It is minimised by choosing a rather short integration interval of eight time bins. The timings of the pulses from the two wire ends differ because of different cable length and signal propagation along the wire. Therefore the phase of the integration interval has to be properly adjusted in order to guarantee the integration over the same part of the pulse on both wire ends.

If a pulse is recognized on the tail of a previous one it is analysed after effects from the previous pulse have been subtracted on the two wire ends independently. For this subtraction a standard pulse shape is determined by averaging a large number of pulses, and then matched in phase and normalised in height to the preceding pulse.

2.4.6 Implementation

The subsystem trigger controller crate (STC, [33]) provides a standard interface to the central trigger electronics (see also section 5.3.5 of reference [1]). The STC in the DC readout is supplemented by a 104 MHz phase locked loop (PLL) card providing an accurate (± 1 ns) clock and a logic card acting as sequence controller. Although responses from the scanner could by simple combination be used directly to respond to the central trigger, inclusion of the logic card in the path allows better overall performance by overlapping some stages of processing with refill and other delays of subsequent events. This places much of the response time of the DC systems in second or even third order dead time, and allows the DC systems to be run at almost full throughput with little or no actual dead time.

The master crate contains interfaces to the CDAQ (VMEtaxi link) and to other crates in that branch (VIC8251) consistent with the common H1 architecture (see Section 7.2.1 of reference [1]). On startup, the master processor loads all other processors with code and data stored in non volatile ram. Once the other processors are running, all communication is made through the buffer memory of the VIC boards connected to each of the remote processors. During a run the master processor operates asynchronously, waiting for an event to be signalled by the trigger processor, and then polling the front end processors until the complete event is ready to be built. The events are not buffered or processed by the master processor.

A monitoring crate provides access to the readout branch for chamber specific control and monitoring systems. A small fraction of the event data can be passed to the monitoring crate for local monitoring, especially that which requires raw data that might be unavailable in the CDAQ monitoring systems. Data is collected from a dedicated memory in the master crate using a differential VSB extension [34] – the VIC8251 connection is not used for technical reasons. Data may also be fed back from the monitoring system into the data stream, to allow important slow control information (e.g. HV, currents) to be recorded together with the event.

The drift chamber readout uses processors of the Motorola 68000 family throughout. These CISC processors are relatively easily programmed at the native instruction level, and all the readout code was written in assembler. By splitting the workload between many processors each fulfilling a specific task it has been possible to avoid the use of an operating system on any of the readout processors. This has minimised response times and maximised performance.

2.5 Proportional chambers

Between 5° and 175° the solid angle seen from the interaction region is completely covered by multiwire proportional chambers. Six independent planes in the forward direction, four in the central and also in the backward direction serve three different functions: to deliver a fast timing signal with a time resolution better than the separation of two succeeding HERA bunch crossings, to provide moderately accurate space points for charged particle track reconstruction at the first level trigger and lastly to add an accurate track element in the backward direction, where the drift chambers fail to provide enough space points.

The planar forward chambers (FWPC) are interspaced between the driftchambers of the FTD described above and are exposed to high particle rates increasing towards the beam pipe. Hence minimum overall thickness and minimal amount of material traversed, sufficient ageing prospects, and cathode pad size adapted to increasing rates near the beam pipe became the primary design criteria. These points do also apply for the two cylindrical chambers in the central region. The inner one (CIP) is closest to the interaction region and covers the largest solid angle. In order not to degrade the track reconstruction of the surrounding drift chambers, the CIP and its outer partner (COP), were fabricated with low mass materials and a narrow active gap. Since the main purpose of the FWPC, COP and CIP is to provide space points for the first level trigger, a pad segmented cathode readout was chosen with graphited surfaces as in other chambers built for high rates [35, 36]. From the reconstructed tracks the event vertex can be deduced and other detector data such as calorimeter and muon information can be validated. Since the trigger logic requests three space points per track, spurious background hits from uncorrelated noise and synchrotron radiation are removed.

In the backward direction the reconstruction of the scattered electron in low momentum transfer events calls for an accurate track segment. This is given by the signals from the four differently oriented anode wire planes of the backward chamber (BWPC). Several wires can be combined for triggering purposes. Standard planar chamber construction techniques sufficed here, since more than one radiation length of electronics and cables from the central tracker separate the BWPC from the interaction region. The BWPC covers the front surface of the backward electromagnetic calorimeter (BEMC) and hence also serves to discriminate electrons and photons.

The properties of all four chamber types are summarized in Table 5. The front end electronics and readout system is identical for all chambers.

	unit	CIP inner/outer	COP inner/outer	FWPC # 1/# 2/# 3	BWPC
active length $\Delta z/\Delta r$[3]	mm	2190	2172	583	515
active zone starts at z/r[3]	mm	-1125	-1107	167	135
mechanical length $\Delta z/\Delta r$[3]	mm	2254	2262	665	597
total length $\Delta z/\Delta r$[1,3]	mm	2467	2360	665	708
thickness $\Delta r/\Delta z$[3,6]	mm	21.5 (25)	30 (34)	40	52 (60)
chamber starts at z/r[1,3]	mm	-1376	-1270	135	110
position of first anode r/z[3]	mm	157/166	501/514	1451/1874/2297	-1423
number of anode planes		1	1	2	4[5]
number of wires		480	1574/1615	724	2496
wire separation	mm	2.1/2.2	2.0	2.5	2.5
gap width	mm	3.0	4.0	4.0	4.0
number of cathode pads		480	288	384	
cathode resistivity	k$\Omega/\square$	$\approx$400	$\approx$ 200	$\approx$300	$\approx$400
length of pad $\Delta z/\Delta r$[3]	mm	36.6	120	13 to 54[4]	
width of pad $\Delta\phi$	°	45	22.5	45 (22.5)[2]	
anode wire tension	N	0.63	0.60	1.5	0.98
plateau length	V	200/250	200	300	200
plateau starts at	V	2425/2375	2900	1900	2800

Table 5: Proportional chamber parameters. The separate columns for CIP and COP refer to the two planes, for the FWPC to the whole module containing two planes.
[1] Inclusive preamplifiers; [2] only for the four outermost of the 20 radial pads;
[3] first coordinate for CIP and COP, second for FWPC and BWPC; [4] width increases with radius, $\Delta r_i = 0.0782 r_i$, where r_i is the inner radius of the pad; [5] the anode wire of each successive plane are rotated by 45°; [7] in active zone (and at end flanges).

2.5.1 Forward proportional chambers (FWPC)

Each of the three chambers in the forward tracker volume consists of two wire planes interleaved with three cathode planes. The gap between the two adjacent cathode planes is 4 mm wide, as indicated in Figure 10. All chamber frames are made of glass fiber epoxy. To reduce the mass in the active area a laminated structure consisting of the following layers is used: 100 μm graphited mylar foil serving as cathode plane, 250 μm printed circuit board carrying 10 μm Cu readout pads, 3.3 mm Nomex [24] mesh, another 250 μm printed circuit board covered with 10 μm Cu for the strips leading from each pad to the preamplifiers on the chamber ends, a further 100 μm of graphited mylar foil in the central plane or aluminized mylar foil on the external planes for electromagnetic shielding. The graphite layers are produced by spraying a mixture of DAG 5466/DAG 213 [37] at 5 bars giving an initial surface resistivity of 1 M$\Omega/\square$, which was reduced to 300 k$\Omega/\square$ by polishing. Each chamber is strengthened by a backplane, 12 mm thick, with two layers of 250 μm glass fiber epoxy sandwiching 11.5 mm Nomex. The overall thickness is 1.7 % of a radiation length. The mechanical tensions of the wires and the foils are supported by 24 and 8 axial rods on the external and internal frames, respectively. The anode planes contain gold plated tungsten wires (Ø 25 μm) spaced by 2.5 mm. They are crimped on pins fixed on the frames. Each wire is connected to the following one through 1 MΩ resistors and to ground through 330 nF capacitors. Groups of 15 wires are connected to separate HV lines, which allows degrading of malfunctioning sectors if necessary. The cathode pads are ring shaped and cover an azimuthal angle of $\pi/8$ each, except for the four outermost of the 20 rings where they cover $\pi/16$. The radial pad width increases with radius in geometrical progression from 18 to 37 mm. Two consecutive cathode planes are offset by one half of a ring, such that the effective polar angle resolution is halved: $r_{min,i+1} = r_{min,i} \times 1.0382$ with $167.5 \leq r \leq 750$ mm. The Pluto gas mixture (see Table 7) was chosen, because the FWPC share their gas volume with the forward drift chambers and transition radiation detectors.

A track crossing all three or at least two modules of the FWPC has to fall into the polar angle range $6.6^\circ \leq \theta \leq 18.0^\circ$ or $5.1^\circ \leq \theta \leq 21.6^\circ$, respectively. For such tracks an effective timing resolution of 20 ns (FWHM) and 47 ns (base width at 10 % of the maximum) was measured using H1 data, well below the required resolution to separate two bunches.

2.5.2 Central proportional chambers

2.5.2.1 CIP The laminar structure of the CIP called for special construction techniques which are described in detail in reference [38].

The double layer of chambers consists of three concentric cylinders. During construction each chamber cylinder was formed on a steel mandril milled to a precision of 25 μm over the full length. The innermost layer of the first cylinder, a 25 μm thick Al-foil provides the electromagnetic shielding. The next layer – 2 mm thick Rohacell foam [14] glued onto the Al-foil with 20 g/m^2 epoxy-glue [39] – gives the chambers the necessary rigidity. The Rohacell surface was polished, and a second 25 μm Al-foil glued to it served as the inner cathode. After cutting the cylinder to the right length the Al-foils were connected to Cu-foils, at the ends and the glass fiber epoxy [6] end flanges were added. These carry the printed circuit boards for the anode wires, which are supported further by glass fiber epoxy rings at 1/3 and 2/3 of the chamber length. The active gap is 6 mm wide. The anode wires (gold plated tungsten, Ø 25 μm) were transfered to the axially prestressed cylinder from planar frames.

The middle cylinder forms the outer cathode of the inner chamber and the inner cathode of the outer chamber. Here the innermost layer, a 20 μm Kapton foil is coated with high resistive graphite (400 k$\Omega/\square$) on one side and 0.5 μm Al on the other side. The Al layer is segmented into pads on which the induced charge on the cathode is collected. The graphite layer in front guarantees a fast disappearance of the accumulated ion charge. This has the advantage, that the readout wires of the pads can be mounted outside the gas volume. After several tests on prototypes [38] the graphite layer in the final chamber was produced by spraying a mixture of DAG213, DAG305 [37] and isobutylmethylketon (IBMK) in a ratio of 20 : 1 : 7 onto the Kapton foil with 3 bar. The cathode foils are again backed by 2 mm Rohacell. The readout wires (150 μm Al) are embedded into 250 μm deep grooves in the Rohacell running along the $z-$axis from the chamber end ($-z$ side) to a hole centered over the pads. The wires were contacted onto the pads with silver paint and soldered at the flange end. Another 20 μm thick Kapton foil with Al-coating is glued onto the Rohacell, which forms together with the wires a wave guide of $\sim 70\ \Omega$ impedance. The Kapton foil again backed by 1 mm Rohacell with a polished surface is covered by another 25 μm Al foil serving as the cathode for the outer chamber. End flanges and connections are similar to those of the first cylinder and the sequence of layers for the third cylinder is identical to that of the second.

Gas sealing is provided by two O-rings at the end flanges (2 mm Ø). The overpressure in the chambers has to be kept small and needs to be monitored carefully in order not to distort the gap. The two chambers have independent gas distributions and are rotated by $\pi/16$ in ϕ with respect to each other, thus halving the eightfold segmentation of each chamber at the trigger level by requiring coincidence of two planes. In z there are 60 pads of 36 mm width in each ϕ sector.

With the gas mixture given in Table 7 the single pad efficiency measured in a test beam was 99 %, while at HERA 94 $\pm$ 2 % was measured with extrapolated jet chamber tracks. From the measured pulse height distributions the gap variations for this light chamber were deduced to be less than 0.2 mm. The measured test beam time resolution (FWHM 21 ns) compares well with the results at HERA. This result converts into a 2 % probability to register a given pad with the wrong (neighbouring) bunch crossing. The probability for crosstalk, i.e. the probability to register signals also in neighbouring pads in z and ϕ and the inefficiencies across the pad boundaries are discussed in detail in reference [38]. The average number of active pads for crossing angles larger than $\theta = 40°$ in a test beam (1.4) compares well with what is observed at HERA.

2.5.2.2 COP The construction of the COP follows closely that of CIP in those aspects concerning the sandwich structure (see Figure 12). Steel mandrils machined to a precision of 60 μm and appropriate to the larger chamber radii were used. To improve the stability of the sandwich structure, the thickness of the core material (Rohacell) was increased to 4 mm. The graphite cathodes (7 m^2 area per chamber) are produced with a screenprinting technique using a resistor ink solution, rather than spraying . The ink [40] has a resistivity of 170 K$\Omega/\Box$ for a 15 μm layer and was diluted with a solvent monobutylic ether of ethylene glycol in a ratio of 1 : 3. A surface resistivity of 200 K$\Omega/\Box$ was obtained after polymerization at 120 °C during 1 hour. The cathode pad structure is provided by gluing patches of 25 μm Kapton coated with 1 μm Cu to the back side of the graphite cathodes, giving an 18–fold segmentation in z and 16–fold segmentation in ϕ. The cathode layer is backed by 3 mm Rohacell, in which 50 μm diameter Cu wires are embedded. A 25 μm Kapton foil coated with 1 μm Cu put on top of the previous layer constitutes with the copper wires the transmission line that carries the chamber signals to the $-z$ end of the chamber. This layer is then backed by 2 mm Rohacell. The Vetronite (G10) end flanges of the chamber support the printed circuit boards to which the anode wires ($\approx$ 1600 per chamber) are soldered and assure the 8 mm chamber gap size. They form the only rigid structure to which the gas distribution and preamplifiers are connected. The three cylinder sandwiches are assembled in vertical position. Pulse height measurements showed that the gapsize variation is of the order of 0.3 mm [41].

Despite its three times larger radius the COP is only moderately thicker than CIP (0.18 % radiation length instead of 0.14 %). The efficiency plateau is reached at 500 V above the CIP plateau with the same gas mixture, a consequence of the larger gap. While in test beams CIP and COP behaved similarly, at HERA the noise level in COP is slightly higher due to more difficult grounding. This requires a higher threshold setting and leads to a typical efficiency of 92 $\pm$ 2 %. The timing resolution is similar to that of the other chambers.

2.5.3 Backward proportional chamber (BWPC)

The BWPC is equipped with five graphited cathode planes (50 μm Mylar foil) and four anode wire planes. It is the only chamber in H1 in which the cathodes are not segmented and the anodes are read out. The graphite coating was fabricated with the same technique as described for CIP. The wires and the foils are stretched between a 23 mm wide inner and a 67 mm wide outer ring of glass fiber epoxy (G10). These rings are 4 mm thick and sustain the active gap of 8 mm per chamber, as indicated in Figure 13. The wires are strung every 2.5 mm, but signals from two neighbouring wires are fed to one preamplifier. The wire orientations are vertical, horizontal and $\pm 45°$ for the four layers. Gas sealing and structural support for the assembly is provided by G10 front and back planes of 10 mm thickness milled down to 6 mm in the active zone. The latter starts at an inner radius of 135 mm and ends at 650 mm, while the whole chamber occupies the region betweenn r = 110 mm and r = 818 mm. The BWPC therefore covers polar angles of $174.5 \geq \theta \geq 155.5°$. The space points given by the BWPC contribute 0.5 mrad to the angular resolution, of the same order as the multiple scattering in the material in front of it. For high energy electrons an efficiency of 87 % per plane was measured from extrapolated CJC chamber tracks. When requiring three out of four planes to be hit in coincidence with the BEMC an efficiency of 98 % is obtained.

2.5.4 Proportional chamber electronics and readout

Preamplifier		Amplifier–Shaper	
Differential gain	65 nV/e	Max. differential gain	400
Rise time (10–90)%	2 ns	Rise time	9 ns
Fall time (10–90)%	20 ns	Pulse width (FWHM)	16 ns
Input impedance	64 Ω	Max. output voltage	3.2 V
Output load	$2 \times 50\ \Omega$	Overload recovery:	
Dynamic range	$\pm$ 300 mV ($\approx 10^7\, e$)	$V_{in} < 5 \times V_{in,sat}$	70 ns
Power supply	$\pm$ 3.5 V (22 mW)	$V_{in} = 30 \times V_{in,sat}$	170 ns
Size	$25 \times 10 \times 2$ mm^3	Power supply	+5, -5.2 V (320 mW)
		Size	$36 \times 3 \times 6$ mm^3

Table 6: Characteristics of the MWPC preamplifier and amplifier–shaper.

A schematic picture of the frontend electronics is shown in Figure 14. The cathode pad signals (CIP, COP, FWPC) and anode wires (BWPC), respectively are preamplified directly on the chambers. A differential signal is then transmitted through a 35 m long cable to the electronic trailer. Each cable contains 16 signal pairs and is connected to a receiver card containing shaping amplifiers, followed by discriminators with computer controllable thresholds. The characteristics of the preamplifier-shaper chain are listed in Table 6. The overall gain can be adjusted to chamber pulse height between 1.3 μV/e and 26 μV/e by means of a resistor on the receiver card. A typical equivalent noise charge is about 3800 e, for a chamber capacity of 60 pF.

The digitized signals are synchronized with the HERA clock and stored in a pipeline constructed from the same gate arrays as used in the muon system (see Section 4.1.4). Upon a first level trigger decision (L1-Keep), the pipeline clock is stopped. A second level trigger decision (L2-Keep) then initiates the data readout. The synchronized pad signals are furthermore made directly accessible to the $z-$vertex and forward ray trigger (see Section 5.3.1.3 of reference [1]). Test registers allow controlling the readout and trigger chains.

The MWPC readout system, an independent branch (# 7) of the H1 data acquisition system (see Figure 22 of reference [1]), is responsible for reading 3936 channels, originating from 270 receiver cards in 15 crates, and some decision data from the two first level triggers. In addition to the frontend crates, the system consists of two standard VMEbus crates and one STC crate [33] in a configuration common to all H1 subsystems (see Section 7.2.1 of reference [1]).

The frontend crates are equipped with a customised 'EasyBUS', which is essentially a simplified 16 bit wide VME bus with a 64 kWord address space lacking any interrupt capabilities but with added analog and ECL signal lines. The latter are used to distribute the clock and L1-Keep signals. The analog lines allow measuring the digitization thresholds loaded to the discriminators through an ADC located on a crate controller (CC) card. The primary task of the CC's is however to connect the crate to a branch driver card (BDC) residing in the master VME crate. The BDC-CC combination maps the EasyBUS address space into the VME frame [42].

Each BDC is directly connected to the STC and contains a DMA (direct memory access) controller and a 4 Kbyte deep FIFO (first in, first out) buffer. An L2-Keep signal can thus initiate a frontend data transfer to the master crate without processor intervention. The maximum transfer speed is 4.5 Mbyte/s. Each of the six BDC's installed in the MWPC area can control eight frontend crates. The latter are grouped into pairs to make use of the 32 bit wide data path of the VME bus. To optimise readout speed, between two and six crates are connected to one BDC.

The first order dead time is determined by the front-end transfer to the BDC as long as the BDC FIFO are not saturated. The saturation rate is given by the average time spent by the data acquisition processor per event. Details of the data acquisition program are available in references [42]. An average time of 4.2 ms per event is needed. This corresponds to an average of 237 hits in 10 bunch crossings.

2.6 Gas systems

To operate the nine different tracking detectors nine separate gas circuits are necessary, with different gas mixtures, flows, and demands on purity and overpressure control. For the forward chambers and CJC closed circuits are used while CIZ, COZ, CIP, COP and BWPC are flushed with premixed gases in open circuits. The main parameters of the gas systems are given in Table 7.

Detector	Gas volume	Gas mixture + additives: volume ratio	Pressure relative to atmosphere		Flow rate		System
			typ.	max.	typ.	max.	circuit
	[l]	[%]	[hPa]		[l/min]		type
Planars+ FWPC	$\sim$900	$Ar/C_3H_8+C_2H_5OH$ (90/10)+1	0.15±0.10	1	1.3	3	I closed
Radials	$\sim$700	Phase I: Ar/C_2H_6 (48/52) Phase II: $Xe/C_2H_6/He$ $+C_3H_7OH$ (20/40/40)+1	0.15±0.10	1	1.0	2	
Radiators	$\sim$500	He/C_2H_6 (60/40)	0.25±0.10	1	0.1	1.5	open
CJC1	$\sim$1140	Phase I: $Ar/CO_2/CH_4$ (89.5/9.5/1)	1.5±0.5	5	1.5	3	II closed
CJC2	$\sim$3080	Phase II: $Ar/C_2H_6+H_2O$ (50/50)+0.5	1.5±0.5	5	4.5	9	
CIZ	$\sim$55	$Ar/C_2H_6+H_2O$ (70/30)+0.2	0.15±0.10	1	0.1	0.6	III open
COZ	$\sim$240	$Ar/C_2H_6+C_3H_7OH$ (48/52)+1	0.15±0.10	1	0.2	0.8	
CIP	$\sim$30	Ar/C_2H_6/Freon12$+H_2O$ (49.9/49.9/0.2)+0.2	0.15±0.10	1	0.07	0.6	
COP	$\sim$150	Ar/C_2H_6/Freon12 (49.9/49.9/0.2)	0.15±0.10	1	0.1	0.6	
BWPC	$\sim$120	Ar/C_2H_6/Freon12 (49.9/49.9/0.2)	0.15±0.10	1	0.1	0.6	

Table 7: The different circuits of the gas systems.

2.6.1 Gas circuits

The simplified diagram of the gas circuit of the planar chambers shown in Figure 15 illustrates the typical features of the gas systems. The system is distributed over three levels, the supply outside the H1 hall, the control room on the first underground floor and finally the distribution rack on top of the electronics trailer near the detector. At the latter point the gas inlet flow for each detector is adjusted by mechanical flow meters and for some chambers split into several streams for further distribution as shown in Figure 15. The static pressure of chambers relative to atmosphere is measured with sensors in the μbar range. In order to avoid too large hydrostatic pressure differences between chambers and sensors, the latter are also located at this point.

From the inlet manifold either pure or premixed gases can be fed into the circuit. Flushing is done by gently filling helium or argon via the two flow meters FL1-1 and FL1-2 into the chambers, while the chamber gas at the same time is sucked out by the membrane pump CP1-1. To hold the chamber pressure during the whole operation within adjustable tolerances of about ± 100 μbar, the solenoid valves SV1-2 and SV1-3 will be either opened or closed depending on the actual pressure inside the detector. As seen from Figure 15, the ingoing and outgoing flows of the chamber gas are split into two paths, one of them containing instruments for continuous gas analysis like infrared meters, a hygrometer and a gas chromatograph in combination with an oxygen trace analyzer. The filling of the chambers proceeds in a similar way as the purging either with premixed gas or by introducing approximately the right proportions of first the non-flammable and later the flammable gases. Then inlet and vent valve are closed and the circuit is switched from the open to the closed mode. The gas circulates through the barrel, the purification units, if needed, through an alcohol or water bath, and through the chambers. Since the purification units absorb part of the gas components, particularly hydrocarbons, a readjustment of the mixture is necessary after typically one day of circulation. To maintain the correct mixture gas can be added to the barrel manually. Repeated circulation for several days, especially when additives like water or alcohol are used, leads then to a homogeneous gas mixture constant in time.

So far three types of additives are used. Some mixtures contain 0.2 % Freon 12 as one of the components of the premixed gas. To other delivered mixtures alcohol (typically 1 %) or water (typically 1000 ppm) is added by passing the gas over a bath of the cooled or frozen liquid stored in a refrigerator in temperature controlled reservoirs. The admixture is adjusted by varying the bath temperature.

2.6.2 Purification and analysis

The closed loop circuits are supplied with purification units for removing oxygen, water and low concentrations of higher organic compounds. For oxygen removal 2 kg BTS-catalyst R3-11 [43] in the reduced state is used as an absorption agent and oxygen levels as low as 20 to 40 ppm have been reached over long time periods. Optimal oxygen removal is obtained with catalyst temperatures of 100 °C to 150 °C. However in the case of ethanol admixture, as is foreseen for the planar chambers, the alcohol will be cracked [44, 45]. Working at temperatures below 80 °C circumvents this problem at the cost of a lower oxygen capacity for the purifier of only about 6 to 15 l [O_2/kg (catalyst)]. A similar problem arises when isopropanol is added to the chamber gas, which is recommended for Stablohm wires and the radial chambers [25, 46]. Since the isopropanol molecule is more fragile than the ethanol molecule, it is cracked even at room temperature into hydrogen and acetone by the catalyst [47]. Use of other O_2-purifiers working at low temperature like Oxisorb [48] and palladium-catalyst [49] give similar problems with alcohol-additives, especially with isopropanol, so that up to now isopropanol could not be used in the closed circuit of the radial chambers.

At room temperature water and higher organic compounds are removed by a mixture of 1.5 kg 3 Å and 0.5 kg 5 Å molecular sieves. In case of water or ethanol additives the molecular sieve eventually saturates, but it is still capable of removing other impurities. Both, molecular sieve and BTS-catalyst are regenerated twice per year or whenever necessary.

Continuous control of gas composition is necessary for constant operation. Infrared meters, dedicated to a certain gas type, but with some sensitivity left for the gas additives give permanent information on changes. Hygrometers in the ppm-range and an O_2-trace analyser allow an early detection of leaks. Complete analysis of the gas composition is performed by an automatic gas chromatograph station, routinely switched into the different circuits. Independently of the use of calibrated gases this instrument gives the different gas portions to an accuracy of ±2 % of the measured value with an overall sensitivity of about 300 ppm [50, 51].

2.6.3 Electronic control and safety

The concept of the H1 gas system control follows the solution chosen for L3 time expansion chamber (TEC) [52, 53]. A Motorola 68000 CPU serves as a crate master, integrated into a VME-system with the necessary resources for monitoring, logging and control equipment. The instantaneous values of all analog outputs of the measuring devices, especially those for pressure and temperature, but also those for supply voltages are controlled within preset limits. Warnings or alarms are generated if one of the relevant parameter values is exceeded. In case of an alarm the gas circulation is stopped and the HV supplies of the detectors concerned are switched off. A computer independent hard wired logic with a more generous alarm setting protects the chambers against destruction in case of program failures or other accidents. In this case also an alarm is generated and the powerless open solenoid valves in the distribution rack on top of the electronic trailer connect the chambers with an argon flushed reservoir at atmospheric pressure as indicated in Figure 15. A set of four independent serial links per gas system monitors all gas parameters and distributes this information to the slow control system (see Section 6 of reference [1]).

Gas sensors are distributed in the H1 detector region, on the electronic trailer with the distribution rack and in the volume occupied by the trackers, as well as in the rooms where flammable gases are handled.

The tracker volume is flushed with $\simeq 12$ m^3 of nitrogen gas per hour to prevent accumulation of flammable gases in case of a leak. Since the operational pressure of most chambers is as low as 0.15 hPa relative to atmosphere and only 1.5 hPa in case of CJC, the amount of gas which may escape through a sudden leak in the chamber region is at most only a few liters. Small continuous leaks are best controlled in the closed loop circuits by measuring the pressure drop in the barrel over several days. The maximum working pressure in these circuits is limited to 1.6 bar absolute. A typical leakage of about 4 l/day corresponds to a pressure drop of ∼40 hPa/day. In the open circuits additional electronic flow controls, in series with FL1-1 and FL1-2, restrict the input flow. In case of a major leak the operational chamber pressure cannot be reached with the low flux adjusted by these controls.

2.7 Scintillators

Both scintillator arrays discussed in this section are located in the backward region (see Figure 3 of reference [1]) and have been installed to reject proton beam associated background at the first trigger level. The present life time of the stored proton beam in HERA during collisions varies between 10 and 48 h. The stored proton current design value is 160 mA with 2×10^{13} circulating protons in total. These protons are lost by beam gas and beam wall interactions producing background showers of energetic penetrating hadrons and halo muons. With a beam life time of 10 h the H1 sensitive detector volume is hit by this background with a frequency of 2.6 MHz.

2.7.1 Time-of-flight counters

The time of flight hodoscope (ToF) consists of two planes of 3 cm thick NE102A scintillator mounted perpendicular to the beam pipe upstream of the interaction region. Particles from proton induced background and from $e-p$ collisions are separated in time at this point by ~ 13 ns. The electron bunches have negligible size whereas the proton bunches are spread over 2 to 3 ns FWHM. The plane nearest to the interaction point (ToF1) lies at $z = -1.95$ m and has 16 butted counters, measuring 317×317 mm^2 thus matching the size of four BEMC stacks. The outer plane at $z = -2.25$ m consists of eight larger counters (317×634 mm^2).

In order to operate inside the 1.14 T field, ToF utilises 24 Hamamatsu R2490-01 high field photomultiplier tubes (PM). It is necessary to mount them perpendicular to the planes of ToF, requiring a light collection countersink to be machined into one of the large faces. A corresponding perspex truncated cone is glued to the other side to match the PM sensitive area. The PM's themselves are housed in non-magnetic holders and held in contact with the small light guide by springs.

Each wall of ToF is made up of a sandwich of scintillator and lead (Figure 16), mounted on a backing plate of non-magnetic steel to minimise stresses from the large magnetic field. The lead is 6.5 mm thick to absorb synchrotron radiation. Steel is used rather than aluminium to minimise eddy currents produced during a magnet quench.

The six inner counters (four on ToF1, two on ToF0) can be moved horizontally up to 20 cm from the beam pipe using computer controlled pneumatic rams. This removes them from the high radiation fluxes around the beam pipe during injection. With the counters in the open position, ToF can be split in half about the horizontal axis, allowing removal without breaking the vacuum in the beam pipe.

Signals produced by the PM's are amplified ($\times 40$), up to ~ 1 V before travelling down 29 m of cable to a NIM logic located in the electronics trailer. Here the signals are discriminated and strobed in three time windows: background, interaction and global, which are used in the first level trigger decision (see Section 5.3.1.1 of reference [1]) available after 250 ns. The device as a whole has a resolution of 4 ns, while individual counters have a resolution of the order of 2 ns. The timing information of all counters is available in the event readout chain.

The setting and width of the time windows greatly affects the performance of ToF, and they are continually updated as offline analysis proceeds. The background window currently starts 18 ns before the centre of the background distribution, and is 25 ns long. The interaction window starts 1 ns after the background window ends and is 13.1 ns long (Figure 17). A constant background of cosmic ray hits is present, about 200 entries per bin. Triggers in the interaction window are in fact much dominated by synchrotron radiation.

2.7.2 The veto wall

In addition to the ToF device two double scintillator veto walls are installed at a distance of 6.5 and 8.1 m, respectively upstream from the interaction point (see Figure 3 of reference [1]).

The smaller inner veto wall covers the near beam area (100×90 cm^2) down to a radius of 11 cm (Figure 16). The four scintillator pairs (NE 114, thickness 6 mm) are read via two photomultipliers (56 AVP, VALVO) each. The pairs are shielded against electromagnetic showers by lead walls of 4 cm thickness. Penetrating particles are then identified by coincidences between two scintillators with a time resolution of $\pm$ 3 ns. The large outer veto wall with an area of ca. 5×4 m^2 overlaps the inner veto wall and nearly all of the liquid argon calorimeter. The array of 10 counter pairs of up to 2.1×0.90 m^2 area each (Figure 16) is grouped around the last upstream HERA quadrupole with a 0.8×0.8 m^2 sized hole. The scintillators (NE 110, 1 cm thick) are coupled to 20 5 inch phototubes of type VALVO XP 2041. These tubes are shielded with thick iron tubes and μ - metal cylinders against the magnetic fringe field (≈ 10 mT).

An iron wall of 5 cm thickness separates the scintillator pairs of the outer wall. The coincidence resolution of such pairs is $\pm$ 8 ns. It is dominated by the light path differences over the large area. The light attenuation length is measured to be larger than 1.5 m and leads to inefficiencies for the detection of minimum ionizing particles of $< 10^{-5}$. (see also references [54, 55, 56]). The time resolution achieved allows a clear time separation between the background of the passing proton beam and event correlated hits during e-bunch passing. A 3 m concrete wall separates the outer veto wall from the main detector and protects it against low energy showers from upstream.

Amplitudes, signal arrival times, rates and efficiencies of all counters are monitored online, and this information is used to study the background condition after each filling and during runs. The time of flight information allows to measure the z position of the $e - p$ interaction point online with a precision of ca. 30 cm. It is used in the first level trigger (see Section 5.3.1.1 of reference [1]), and is sent to the central data acquisition system for off-line analysis.